

# STATS 1 - JUNE 2014

① a) i) Mode = 71

Range = 75 - 66 = 9

ii)

x	f	CF
66	1	1
67	2	3
68	3	6
69	5	11
70	7	18
71	8	26
72	4	30
73	2	32
74	2	34
75	1	35

Median =  $\frac{35+1}{2} = 18^{\text{th}} = 70$

LQ =  $\frac{35+1}{4} = 9^{\text{th}} = 69$

UQ =  $\frac{3(35+1)}{4} = 27^{\text{th}} = 72$

IQR = 72 - 69 = 3

iii) From calc:  $\sum x = 2464$

$\bar{x} = 70.4$

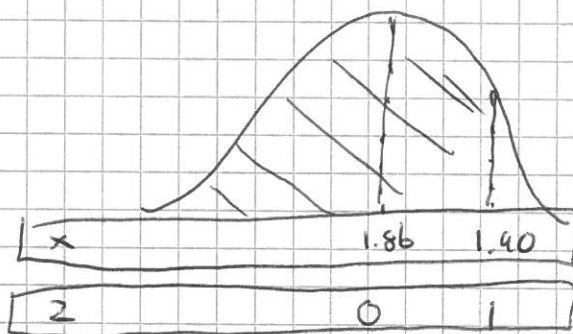
$s = 2.06083$

b) She keeps  $(x - 60) \rightarrow \bar{x} = 70.4 - 60 = 10.4$

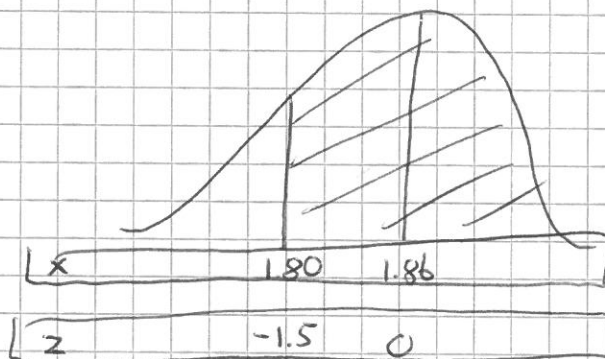
$s$  is unchanged at 2.06083

②  $X \sim N(1.86, 0.04)$

a) i)  $P(X < 1.90)$   
 $= P\left(Z < \frac{1.90 - 1.86}{0.04}\right)$   
 $= P(Z < 1)$   
 $= 0.84134$



ii)  $P(X > 1.80)$   
 $= P\left(Z > \frac{1.80 - 1.86}{0.04}\right)$   
 $= P(Z > -1.5)$   
 $= P(Z < 1.5)$   
 $= 0.93319$



$$\begin{aligned}
 \text{iii) } P(1.80 < X < 1.90) &= P\left(\frac{1.80 - 1.86}{0.04} < Z < \frac{1.90 - 1.86}{0.04}\right) \\
 &= P(-1.5 < Z < 1) \\
 &= P(Z < 1) - P(Z < -1.5) \\
 &= 0.94134 - (1 - 0.93319) \\
 &= 0.77453
 \end{aligned}$$



iv)  $P(X \neq 1.86) = 1$

b)  $X \sim N(1.86, \sigma^2)$   
 $P(X > 1.80) = 0.98$   
 Look up Z value for 0.98  
 $= 2.0537$



Standardize:

$$\frac{1.80 - 1.86}{\sigma} = -2.0537$$

$$\text{Rearr } \frac{1.80 - 1.86}{-2.0537} = \sigma = 0.02921$$

- ③ a) i)  $P(F) = 220/750 = 0.293$   
 ii)  $P(A \cap B) = 24/750 = 0.032$   
 iii)  $P(A \cup B \text{ but not both}) = \frac{110 + 215 - 24 - 24}{750} = \frac{277}{750} = 0.369$   
 iv)  $P(G|F) = \frac{64}{220} = 0.291$   
 v)  $P(F|G) = \frac{64}{195} = 0.328$

b)  $P(DB \cap DB \cap MG) = \frac{92}{750} \times \frac{91}{749} \times \frac{55}{748} = 0.00109$

But, There are 3 ways this can happen

$$\rightarrow 3 \times 0.00109 = 0.00327$$



④ a) i) From calc:  $r = 0.91468\dots$

ii)  $r = 0.91468$  as linear scaling does not affect the value of  $r$

b) There is a very strong, positive, linear correlation between average qualifying speed & average race speed.

⑤ a) i)  $OH \sim B(30, 0.18)$

$$P(OH = 3) = 30C3 \times 0.18^3 \times 0.82^{27} \\ = 0.11151$$

ii)  $H \sim B(30, 0.1)$

$$P(H \leq 5) = 0.9268 \quad (\text{from table})$$

iii)  $H \sim B(30, 0.35)$

$$P(H > 10) = 1 - P(H \leq 10) \\ = 1 - 0.5078 = 0.4922$$

iv)  $H \sim B(30, 0.25)$

$$P(5 < H < 10)$$

can be: 6, 7, 8, 9

$$= P(H \leq 9) - P(H \leq 5)$$

$$= 0.8034 - 0.2026 = 0.6008$$

b)  $H \sim B(150, 0.72)$

$$\text{Mean} = np = 150 \times 0.72 = 108$$

$$\text{var} = np(1-p) = 150 \times 0.72 \times 0.28 = 30.24$$

⑥ a) i)  $a = 15$  as no pressure applied when  $z = 0$

ii) From calc:  $a = 14.90968\dots$

$$b = -0.02093\dots$$

$$\rightarrow y = 14.91 - 0.03z$$

iii) When the pressure increases by 1, the seal depth decreases by 0.03 cm.

b)  $x = 225 \rightarrow y = 14.91 - 0.024(225)$   
 $= 9.37442\dots$

c) i) 400 is outside the range of the data,  
so we would be extrapolating.

ii)  $x = 525 \rightarrow y = 14.91 - 0.024(525)$   
 $= -0.33226$

Impossible to have a negative steel depth.

① a) i) Try 2 standard deviations from mean  
 $\rightarrow 118 - 2 \times 65 = -12$

We would expect some data here, and yet it is impossible to have negative volume.

ii) Sample size  $> 30$ , therefore we can apply the Central Limit Theorem.

b) i)  $\bar{x} = 118$      $s = 65$      $n = 80$

98% z value (two tailed) = 2.3263

$\rightarrow \mu = \bar{x} \pm z \times s/\sqrt{n}$

$\mu = 118 \pm 2.3263 \times 65/\sqrt{80}$

$= 118 \pm 16.4057\dots$

$= (101, 135)$

ii) 140 lies outside confidence interval.

Therefore the claim seems unlikely to be true.